CONTRIBUTION FROM THE CHEMICAL TECHNOLOGY DIVISION, OAK RIDGE NATIONAL LABORATORY, OAK RIDGE, TENNESSEE

Preparation of MF_6 ·NaF Complexes with Uranium, Tungsten, and Molybdenum Hexafluorides¹

By SIDNEY KATZ

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The hexafluorides of uranium, tungsten, and molybdenum react with sodium fluoride to reach 1:2 and 1:1 stoichiometric ratios with unexpected speed when the sodium fluoride has been formed by decomposition of UF₆:2NaF. The equilibrium pressures of the newly prepared 1:1 complexes for the reaction $2(MF_6:NaF) \Rightarrow MF_6 + MF_6:2NaF$ are: for UF₆, log $P_{mm} = 11.06 \pm 0.02 - (3.48 \times 10^3)/T$; for WF₆, log $P_{mm} = 7.05 \pm 0.02 + (1.99 \times 10^3)/T$; for MoF₆, log $P_{mm} = 7.29 \pm 0.03 - (1.83 \times 10^3)/T$.

Introduction

This report describes the preparation by gas-solid reactions, of solid complexes of sodium fluoride with uranium hexafluoride, tungsten hexafluoride, and molybdenum hexafluoride of the formula type MF_6 ·NaF and the measurement of the equilibrium pressures of the metal hexafluorides over these complexes. An improved preparation of compounds of the type MF_6 ·2NaF, previously reported,² is also presented.

For the previously reported² preparation of UF_{6} · 2NaF, WF₆·2NaF, and MoF₆·2NaF, the metal hexafluoride was sorbed upon a sodium fluoride prepared by decomposing NaF·4HF. Metal hexafluoride in excess of that needed to form the MF₆·2NaF compound sorbed slowly and incompletely even at lower temperatures. A subsequent observation that metal hexafluorides sorbed better upon sodium fluoride formed by decomposing UF₆·2NaF led to the work reported here.

The compound UF₆·NaF has already been prepared by Malm and Selig³ by reaction of uranium hexafluoride with sodium fluoride suspended in fluorocarbon (C_7F_{16}). They report a decomposition pressure of about 35 mm at 100° (in agreement with data presented here). The similar compounds CsUF₇, CsWF₇, CsMoF₁, NH₄UF₇, NH₄WF₇, and NH₄MoF₇ have also been reported.^{4,5}

Experimental Section

Materials and Gasometric Apparatus.—These are as described previously.²

Preparation of the Sodium Fluoride Complexes with Hexafluorides of Uranium, Tungsten, and Molybdenum.—The procedures are as described previously² except for the preparation of the sodium fluoride sorbent and the temperatures at which the sorptions were conducted.

The sodium fluoride sorbent was prepared by either of two methods, which differed in the manner of the preliminary formation of the complex UF₆·2NaF which was to be subsequently decomposed. The first method for preparing the preliminary UF₆·2NaF was by uranium hexafluoride sorption after hydrogen fluoride treatment of the sodium fluoride, as described previously.² The second method for preparing the preliminary UF₆·2NaF consisted in successive sorption-desorption cycles of uranium hexafluoride on 270-mesh sodium fluoride without any prior hydrogen fluoride treatment. The uranium hexafluoride sorption curves for each of these preparative methods are shown in Figure 1; the first method was preferred because it was faster and required fewer manipulations. The preliminary UF₆·2NaF, thus prepared, was then decomposed by heating to 350° at low pressure to remove gaseous uranium hexafluoride while leaving the solid relic of the former solid complex; a final treatment of the residue with fluorine at 200 mm and at 350° removed traces of uranium. Surprisingly, the surface area of sodium fluoride so prepared was little different from that made by hydrogen fluoride treatment alone.²

The critical importance of temperature of sorption, noted in the previous work,² for preparation of the MF₆·2NaF compounds no longer prevailed with the sodium fluoride made by the improved technique; the sorptions proceeded very rapidly at all temperatures tested, provided that the gas pressure exceeded the decomposition pressure of the compound formed. In the upper section of Figure 2 are presented comparisons of the previously reported sorptions,² each at the optimum temperature, with sorptions at 150° for each of the metal hexafluorides using the improved sodium fluoride. In the lower section of Figure 2 are shown the sorption curves for the preparation at temperatures of 60 to 80° of the MF6 NaF complexes discussed here. These complexes may be prepared in two steps, using successively lower temperatures, or in one step at the lower temperature. Two-step sorptions, using different metal hexafluorides at each step, were successful where uranium or tungsten hexafluoride was the second gas; the temperatures and curve forms were similar to those shown in Figure 2 for those gases.

Results

Gasometric and Chemical Analyses.—The gasometric ratios NaF/MF_6 shown in Figure 2 are (previous results¹ given in parentheses for comparison)

Hexafluoride	Ratio after first step	Ratio after second step
UF_6	2.00(2.01)	1.00
WF_6	2.00(2.11)	1.04
MoF_6	2.01(2.24)	1.05

The concentrations of uranium, tungsten, and molybdenum found in the final product compare with the theoretical values as

	% U in	% W in	% Mo in
	$UF_6 \cdot NaF$	WF6 · NaF	MoF6 · NaF
Found	58.9	52.1	35.1
Theoretical	60.4	54.1	38.1

As in the previous work,² the metal contents are systematically low because of nickel impurity introduced from the sample tray and because of water pickup; the

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Figure 1.—Sorption of UF₆ on HF-treated and on untreated NaF to prepare UF₆ \cdot 2NaF.



Figure 2.—Comparisons of MF_6 sorptions by previous and new techniques to obtain MF_6 ·2NaF and completion of sorption to obtain MF_6 ·NaF.

bias is slightly larger here because the fluorine treatment was more rigorous (causing more nickel metal to be converted to the fluoride), and the product more readily reacted with atmospheric moisture.

Equilibrium Pressures of the MF_6 ·NaF Complexes.— The equilibrium pressures, measured as described,² and the corresponding solid compositions and temperatures are presented in Tables I–III and are plotted in Figure 3

	TABLE I		
UF6 PRESSURES OVER UF6.2NaF-UF6.NaF SOLID PHASES			
	Solid composition, a	Press of	
Temp, °€	mole ratio NaF/UF6	UF6, mm	
69	1.008	8	
78	1.009	13	
83	1.013	18	
83	1.026	20	
98	1.038	50	
99.5	1.082	52.5	
110	1.072	92	
114	1.093	114	
121	1.266	166	
121.5	1.269	170	
123	1,443	180	
123.5	1.185	188	
124	1.192	194	
125	1.385	192	

 $^{\alpha}$ By gas evolution measurements assuming $\mathrm{UF}_{6}\text{\cdot}\mathrm{NaF}$ as initial solid.

	TABLE 11	
WF6 PRESSURES	over WF6.2NaF-WF6.N	aF Solid Phases
Temp, °C	Solid composition, ^a mole ratio NaF/WF6	Press of WF6, mm
67	1,761	16
67.5	1.718	17
83	1.037	27
96	1.026	41
109	1.074	68
123.5	1.916	105
137	1.675	156
137	1.387	160
139	1.115	163
139	1.401	171

 $^{\alpha}$ By gas evolution measurements assuming $WF_{6}{\cdot}\operatorname{NaF}$ as initial solid.

	TABLE III		
MoF_6 Pressures over $MoF_6 \cdot 2NaF - MoF_6 \cdot NaF$			
Solid Phases			
	Solid composition, ^a	Press of	
Temp, °C	mole ratio NaF/MoF_6	MoF6, mm	
45	1.026	34	
54	1.039	51	
72	1.076	93	
73	1.165	94	
74	1.277	98	
75	1.304	120	
90	1.368	178	

 a By gas evolution measurements assuming ${\rm MoF}_6{\cdot}\,{\rm NaF}$ as initial solid.



Figure 3.—Equilibrium pressures of MF_6 over $MF_6 \cdot 2NaF-MF_6 \cdot NaF$.

in the conventional way, $\log P_{\rm mm} vs. 1/T$, along with the straight line fitted by the least-squares method. The equations for the lines and the calculated enthalpy changes (kcal/mole of evolved gas), assuming no substantial solid solutions, are

$$\begin{split} \log P_{\rm mm} &= 11.06 \pm 0.02 - (3.48 \times 10^{8})/T; \\ \Delta H &= 15.9 \pm 0.2 \quad ({\rm UF_6~over~UF_6\cdot NaF}) \\ \log P_{\rm mm} &= 7.05 \pm 0.02 - (1.99 \times 10^{3})/T; \\ \Delta H &= 9.1 \pm 0.2 \quad ({\rm WF_6~over~WF_6\cdot NaF}) \end{split}$$

$$\log P_{\rm mm} = 7.29 \pm 0.03 - (1.83 \times 10^3)/T;$$

$$\Delta H = 8.4 \pm 0.4 \quad ({\rm MoF}_6 \text{ over MoF}_6 \cdot {\rm NaF})$$

for the reaction $2(MF_6 \cdot NaF) \leftrightarrows MF_6 + MF_6 \cdot 2NaF$.

Evidence for Absence of Solid Solutions.—The data of the preceding section demonstrate the interdepend-

ence of system temperature and MF_6 gas pressure independently of solid composition for solid compositions both close in composition to MF_6 ·NaF (mole ratios less than 1.03) and different (see Tables I–III). A similar condition was evidenced in the previous paper² for the system MF_6 ·2NaF.

Also, the MF_6 pressure over the stoichiometric composition ($MF_6\cdot NaF$) was raised isothermally (at a temperature where the equilibrium pressure over the $MF_6\cdot NaF-MF_6\cdot 2NaF$ pair is less than 1 mm) to 200 mm without altering the solid composition as measured by gas inventory changes.

Furthermore, the temperature of the system containing the stoichiometric composition (MF_6 ·NaF) was decreased in the presence of 200 mm of MF_6 without altering the solid composition; the solid composition remained unchanged during the subsequent temperature rise in the presence of less than 1 mm of MF_6 . For these tests the temperature was cycled through the complete interval permitted by vapor pressures of liquid MF_6 and equilibrium pressures of the MF_6 · NaF- MF_6 ·2NaF pairs (approximately 50° interval).

Equilibrium Pressures of Mixtures of MF_6 ·NaF Complexes.—The equilibrium pressure data for the mixture of UF_6 ·NaF and WF_6 ·NaF fell into a single family of points, regardless of the order of sorption of the uranium and tungsten hexafluoride. The curve obtained for that mixture is presented in Figure 4, compared with the curves for the separate complexes and a calculated curve for the sum of the separate complexes.

The equilibrium pressure data for mixed UF_6 ·NaF with MoF₆·NaF and mixed WF₆·NaF with MoF₆·NaF fell on the curve for MoF₆.NaF and are not shown. (The summation curves are both so close to MoF₆·NaF that they could not be distinguished.)

Conclusions

The complexes UF_6 ·NaF, WF_6 ·NaF, and MoF_6 ·NaF and the three equimolar mixtures of the complexes have been prepared by gas-solid reactions. Their successful preparation depended upon the pretreatment of the sodium fluoride.

The empirical formulas for the complexes are derived from the stepwise formation of the MF_6 ·2NaF and MF_6 ·NaF compounds, chemical analyses of each product, and the specific equilibrium pressure curve for each complex. The absence of other steps or other



Figure 4.—Equilibrium pressures for mixed complexes; experimental and calculated values compared to equilibrium pressures of component complexes.

equilibrium pressures at other ratios precludes the presence of other complexes. The temperature, pressure, and solid composition data indicate absence of solid solutions for the compounds UF_6 ·NaF, WF_6 ·NaF, and MoF_6 ·NaF.

An indication of whether the mixed complexes are solid solutions or exist with complete absence of interaction may be inferred from the comparisons of the measured curves to curves for the individual complexes and to curves produced by plotting sums of the pressures of the individual complexes. From these data it appears that the UF₆·NaF–WF₆·NaF mixture lies between the two states but closer to the condition of complete absence of interaction. The two mixed complexes, UF₆·NaF–MoF₆·NaF and WF₆·NaF–MoF₆· NaF, both appear to satisfy the conditions for complete absence of interaction.

The failure of molybdenum hexafluoride to sorb well on either the UF₆·2NaF or the WF₆·2NaF appears due to the relative instability of the MoF₆ complex in each series of complexes.

The superior sorption characteristics of the uranium hexafluoride treated sodium fluoride appear to result from the retention in the solid sodium fluoride of position vacancies formerly occupied by the uranium hexafluoride.

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